

**Display Fountain, System, Array and Wind Detector**

5           The present invention relates to fountains, particularly display fountains, although the invention in its different aspects may also have other applications.

10          Display fountains come in many shapes and sizes. Water "features" are a common and increasingly popular aspect of domestic garden scenery. Larger displays are frequently employed in public places and have long been an adjunct to architectural or sculptural works. Most fountains are static, in that they have a single mode of operation - they are either on, or off. Static fountains are the simplest and least expensive, and generally only 15 require a pump or water supply to operate. These kinds are affordable by most people and are seen in many garden ponds. Various nozzles provide different effects from sprays to jets, and may be arranged to entrain air so that a foaming spray is generated.

20          However, more sophisticated fountains are dynamic in that their operation is controlled, and accordingly varied, by different jets being switched on or off, or having their pressures varied, or redirected. The control arrangement is invariably electronic with greater 25 or lesser complication, and involves the use of selectively operable mechanical valves that can interrupt flow, as may be desired. By this means a wide variety of different effects can be achieved. But such variety comes at a significant cost, not just in terms of price, 30 but also of reliability. Fountains generally involve recycling pond or fountain pool water, and debris eventually builds up and can block valves etc.

One recent development in fountain displays is the use of slugs of water. Although a continuous jet of water involves continuous motion, this fact disguised by a complete arc of a water jet, which can appear somewhat static. If, however, slugs of water are generated, which slugs have a beginning and an end, the motion is brought home to the viewer. US-A-5979791 and US-A-6119955 both disclose arrangements for producing slug jets, one involving the use of a syringe-type of arrangement, and the other involving a plug rapidly releasing and closing an orifice of a chamber containing liquid under pressure.

US-A-5918809 discloses a water display arrangement in which a float is provided with nozzles supplied by flexible water pipes, the reaction from the nozzles moving the float about on a pond or pool surface and creating interesting effects. However, mechanical switching arrangements are provided.

Numerous patents disclose fluidic arrangements for producing oscillating jets, whose main application appears to be in the automotive field for vehicle windscreen and headlight washing. Examples are to be found in US-A-6253782, US-A-5213269, US-A-5181660, EP-A-0208174 US-A-4398664, US-A-452867 and WO-A-7900361.

EP-A-0331343 discloses the use of a fluidic bistable oscillator in the production of a spray of droplets having a narrow size spectrum. SU-A-478622 discloses a display fountain using a diverter to provide alternating jets under pneumatic control.

It is an object of the present invention to provide a display fountain that has opportunities for a variety of functions without the necessity of moving valves, pistons or the like mechanical components.

In accordance with a first aspect of the present invention there is provided a fountain comprising:

a supply of water under pressure;

5 a primary fluidic diverter having an input for said supply, and first and second outputs diverging from said input, two control ports provided with control flow to direct input flow to one or other of said outputs; and

10 a vortex amplifier comprising a vortex chamber, a radial port, a vortex inducing port and an axial port; wherein one of said first and second primary diverter outputs is connected to said vortex inducing port and the other is connected to said radial port, said axial port leading to a nozzle whereby an alternating vortex spray or axial jet is produced. Accordingly, when the diverter switches flow to the vortex inducing port of the vortex amplifier, a vortex is induced in the vortex chamber so that flow issuing from the nozzle swirls and forms a conical spray. However, when the diverter switches flow to the radial port of the vortex amplifier, no vortex forms in the vortex chamber, the flow therein being only radial, whereby a non-swirling axial and coherent jet issues from the 15 nozzle.

20 Preferably, said control ports are interconnected by an inertia loop, whereby oscillations are induced in the control flow to switch flow alternately between said first and second outputs.

25 Alternatively, said outputs may have restrictors therein and include feed back loops into said control ports, whereby oscillations are induced in the control flow to switch flow alternately between said first and second outputs.

Said first and second outputs of either diverter may be vented to isolate each input from the outputs, and the outputs from one another.

Any of said diverters may be cusped between said 5 first and second outputs to increase stability of flow through said first and second outputs.

Preferably, said vortex amplifier comprises an annular chamber formed by a tubular housing and central body, supply flow to the amplifier entering said annular 10 chamber at one end, the other end of the annular chamber being terminated by a nozzle plate defining with said central body said vortex chamber, said housing having an opening forming said vortex inducing port.

Said vortex inducing port is preferably a passage 15 from a supply chamber outside said housing and arranged tangentially with respect to said vortex chamber. Alternatively, said vortex inducing port comprises a plurality of said openings in said housing, each opening provided with a vane to tangentially direct radial inflow 20 from a supply chamber surrounding said housing.

Preferably, said nozzle is interchangeable with different nozzles displaying one of various spray patterns when vortex spray issues therefrom.

A spray catcher may be disposed beyond the nozzle to 25 deflect vortex spray issuing from said nozzle, the catcher having an orifice to permit passage of said axial jet to flow unimpeded. Indeed, the catcher may be formed as an inverted cup, so as to destroy entirely said vortex spray, although still permitting the jet flow.

Alternatively, said nozzle may open into an annular diffuser to catch said vortex spray, but not said axial jet, said diffuser opening into an annular pressure plenum. The plenum may be provided with discrete nozzle 5 exits. These can produce discrete jets and they may be spaced around the central jet to produce a crown-like spray, alternating with the central, axial jet. On the other hand, the nozzle exits may be employed for switching of other elements of a fountain system.

10 Two vortex amplifiers may be provided in parallel, each with its own supply to its radial port, each vortex inducing port being connected to one or other of said first and second outputs of the primary diverter.

Indeed, such an arrangement may also be provided as 15 a component of a fluidic control arrangement in a fountain system wherein, instead of said axial outputs of the two vortex amplifiers leading to nozzles, they lead to further components of the system, and which are arranged to be controlled by greater or lesser flow rates 20 from the vortex amplifiers that issue from said axial output depending on whether there is flow into said vortex inducing port.

Alternatively, or in addition a fountain system may include two primary diverters whose first outputs are 25 joined together and comprise the radial input for said vortex amplifier, and whose second outputs are connected to separate vortex-inducing ports of said vortex amplifier, whereby several modes of operation of the vortex amplifier results. To achieve variety in the 30 display, the diverters are preferably arranged deliver flow at different strengths, either by being different in size or of supplied pressure and/or flow. The diverters

could be designated "strong" and "weak". For example, when the vortex inducing ports are arranged to induce a vortex in the same direction with respect to one another, then column A in the following table shows the resulting 5 flow states in the axial outlet of the vortex amplifier. The first two columns indicate the direction in which the diverters are switched (to first or second outputs). Four possible circuit states are produced, ranging from one (first row) with zero swirl (and a strong coherent 10 jet) to one with maximum swirl (fourth row, with both diverters inducing vortex flow). The others have intermediate swirl strengths (partial swirls 1 and 2 being different) giving a total of four possible water jet or spray effects.

15 Alternatively, if the vortex inducing ports are arranged to oppose one another, then the four possible flow states are as tabulated in column B. They range between zero swirl (row 1) and a high swirl state (rows 2 or 3 depending on the relative strengths of the diverter 20 flows). This high swirl state has less swirl intensity than that of column A. The fourth row, corresponding to both diverters attempting to induce vortex flow in opposite directions produces another intermediate swirl state. Consequently this "contra-swirl" configuration 25 produces a finer gradation of swirl intensity than that with co-directional vortex inducing ports. Small degrees of swirl cause great degrees of effect in the jet efflux. The relative swirl strengths of the partial swirl states depend on the relative strengths of the two diverters but 30 this relativity or ranking is unimportant. The significant attribute is the ability to produce four distinct display phenomena.

Diverter 1, Output in flow	Diverter 2, Output in flow	1.1.1A Axial output from Vortex amplifier	1.1.2B Axial output from Vortex amplifier
First	First	Non-swirl flow	Non-swirl flow
Second	2. First	Partial swirl 1	Partial swirl 1
First	Second	Partial swirl 2	Partial swirl 2
Second	Second	Maximum swirl	Partial swirl 3

Table I

If the diverters are themselves controlled to switch at different times, the period of each phase can vary and appear somewhat random. This can be achieved, for 5 example, by a control loop for each diverter having a different length, given that it is primarily the length of such loop that controls oscillation period.

A novel form of self oscillating vortex nozzle having potential application in a fountain system 10 according to the first aspect of the present invention comprises a cylindrical vortex chamber having a central output nozzle and an input comprising a section of the cylindrical wall of the chamber to which an input chamber is connected, a narrowing of the input chamber being 15 provided at the input section of the vortex chamber, whereby flow entering the vortex chamber oscillates between swirling entry and straight radial entry leading to oscillations in the out put between a straight jet and a swirling spray.

20 Windy conditions adversely affect the appearance of fountains, and frequently causes loss of water from a surrounding pool, which might be problematic in respect both of the loss of water from the pond or pool, as well as wetting surrounding areas.

Consequently, in its first aspect, the invention also provides a wind detection and adjustment device comprising a catcher for water issuing from a detecting jet and falling under no-wind conditions, and a wind control diverter having a supply input, first and second wind control outputs diverging from said supply input, two wind control ports to direct supply input flow to one or other of said outputs, wherein water caught by the catcher is supplied to one control port to direct supply input flow to said first wind control output, the other control port being supplied from a feedback loop from said first wind control output that switches supply input flow to said second wind control output when no water flows from said catcher.

Preferably, said first wind control output is connected to the radial port of a fountain supply vortex amplifier to provide a strong flow therethrough, and said second wind control output is connected to a tangential port of a vortex amplifier to provide a weak flow therethrough, output from the fountain supply vortex amplifier supplying the fountain display.

Indeed, from a second aspect, the present invention provides a wind detection device comprising a catcher for liquid issuing from a detecting jet and falling under no-wind conditions, an outflow from the catcher, and means to detect liquid in the catcher.

Said means to detect may comprise a pressure sensor sensitive to hydrostatic pressure of liquid in the catcher. Alternatively, said means to detect may comprise a flow detector sensitive to outflow of liquid from the catcher.

Inherent in such a detection device is that, in high-wind conditions less liquid falls into the catcher, so the outflow from it, or the hydrostatic pressure in it, is less than in no-wind conditions. Ultimately, in 5 high-wind conditions, outflow from the catcher leads to both the hydrostatic pressure and outflow reducing to zero. Whether this occurs very rapidly, so that the detector is sensitive to gusts, or slowly, so that the detector is sensitive only to sustained high-wind, is a 10 matter of design choice. Indeed, there is no reason why the pressure or outflow detectors should not be sensitive enough to detect gradations of wind.

The wind detector is most suitable where there is already a source of liquid under pressure, such as in 15 fountain displays. In this event, and others, the liquid is preferably water. The detecting jet is preferably vertical, although it may be pointed in any direction provided the catcher is positioned to receive the detecting jet in no-wind conditions. The jet may be 20 vertically down. The wind detector may be employed with a fountain display according to the first aspect of the present invention, but equally it could be employed with more conventional display fountains employing 25 electrical/mechanical controls. Thus the flow/pressure detectors may be non-fluidic.

Preferably, manual control of a fountain display in accordance with the first aspect of the present invention is provided, comprising a manual diverter having a manual input, first and second manual outputs diverging from 30 said manual input, first and second manual control ports to direct said input flow to one or other of said outputs, wherein each control port is supplied by a branch from said manual supply, each branch being

controlled by a first restrictor and at least the first control port branch having a second restrictor, a selectively blockable vent being provided between said first and second restrictor whereby, when said vent is 5 blocked, said restrictors are such that control flow is primarily through said first manual control port and, when said vent is not blocked, control flow is primarily through said second port.

Both branches may have a second restrictor, and both 10 having a selectively blockable vent between said first and second restrictors in each case.

A pilot diverter may be provided, comprising a pilot flow input, first and second pilot outputs diverging from said pilot input, two pilot control ports provided with 15 control flow to direct pilot input flow to one or other of said pilot outputs, which pilot outputs comprise the control ports of said primary diverter.

Multiple logic diverters may be connected in a logic circuit wherein each diverter has a logic flow input, 20 first and second logic outputs diverging from said logic input, two logic control ports provided with control flow to direct logic input flow to one or other of said logic outputs, which logic outputs comprise the control ports of any other logic diverter, any pilot diverter or said 25 primary diverter.

Said pilot diverter may be in the form of a logic module receiving a plurality of inputs from different sources whereby the direction of switching of said primary diverter may be dependent on a plurality of 30 factors controlled by said logic module.

A fountain display in accordance with the first aspect of the present invention may comprise a plurality of diverters, some providing alternating jets directly, and others feeding vortex amplifiers providing 5 alternating jets and sprays, each diverter being controlled by said logic module having a number of inputs, one of said inputs being connected to one output of a neighbouring diverter, and another of said inputs being connected to the other output of said neighbouring 10 diverter or to one output of a different neighbouring diverter.

A neighbouring diverter for a diverter on one side of the fountain display may comprise a diverter on the opposite side of the display, whereby the display is 15 topologically on the surface of a sphere.

Said diverters may be arranged in a square formation and each diverter may have eight neighbours, said logic module having four inputs on one side and four on the other.

20 However, in a third aspect of the present invention, there is provided a fountain display, comprising at least two display elements, each element being driven by at least one output of a diverter directly associated with each element and controlled by a logic module, each 25 diverter comprising an input for a supply of liquid, and first and second outputs diverging from said input, and at least one control port selectively provided with control flow to direct input flow to one or other of said outputs, and each logic module having at least two inputs 30 and at least one output connected to the control port of the diverter to provide said control port with said selective control flow, and wherein at least one output

of the diverter of one element is connected to one input of the logic module of another element.

Preferably, each element has two modes of operation, one mode driven by one output of said associated diverter and the other mode being driven by the other output of said associated diverter, said connection to said input of the logic module of said another element being a branch of one of said outputs of said associated diverter.

Said logic module may comprise multiple logic diverters in a logic circuit, wherein each logic diverter has a logic flow input, first and second logic outputs diverging from said logic input, two logic control ports provided with control flow to direct logic input flow to one or other of said logic outputs, which logic outputs supplies the control ports of any other logic diverter, or the, or one, output of the logic module.

The display elements may be in a formation in which each element is surrounded by  $N$  neighbouring ones of said elements and in which each logic module has  $N$  inputs, one from said branch of each neighbour. The formation might be square, and  $N$  might be eight. Indeed, the number  $N$  of neighbours and inputs may be the same for each element, the display being arranged as a topological sphere.

In one embodiment, the display arranged to emulate a cellular automaton demonstrating the "Life" process of J H Conway. In another, it is arranged to emulate a cellular automaton demonstrating the "rule 30" algorithm of S Wolfram.

In a different aspect, the present invention also provides A fountain comprising: a supply of water under

pressure; a fluidic diverter having an input for said supply, first and second outputs diverging from said input, and two control ports provided with control flow to direct input flow to one or other of said outputs; a 5 control loop interconnecting said control ports to cause oscillation of said direction of the input flow; and a tapping in said control loop, whereby said control loop may be supplied with water and/or drained of water to control the frequency of said oscillation.

10 Preferably, said tapping is a first tapping connected to said supply, a second bleed tapping being provided in the control loop between said first tapping and one control port, whereby said first tapping admits flow into the control loop, said second tapping drains 15 flow from said control loop, whereby switching of the diverter may be controlled by restricting said drainage. Restrictors may be provided around said second tapping to adjust relative flow in the control loop on either side of the second tapping, and into the bleed.

20 The diverter may be arranged to be monostable to one of said output ports, temporary blocking or unblocking of said bleed tapping serving to switch flow to the other of said output ports.

25 Embodiments of the invention are further described hereinafter, by way of example, with reference to the accompanying drawings, in which:-

Figures 1a to f are schematic illustrations of diverters useful in the practice of the present invention;

30 Figures 2a to d are a schematic illustration of a diverter controlled by a pilot diverter, its symbolic

representation, a circuit involving two such diverters, and a multi-stage register, respectively;

Figures 3a to d are a side section, section on the line 1-1 in Figure 3a, section on the line 2-2 in Figure 5 3a, and a perspective view of a vortex valve useful in the performance of the present invention;

Figures 4a,b and c are side sections through nozzle arrangements useful with the vortex valve in Figure 3;

Figures 5a,b and c are side views of adaptations of 10 the nozzles in Figure 4 and provided with swirl catchers.

Figures 6a to g are side section and perspective views of different nozzle arrangements;

Figures 7a to d show variations of the vortex valve of figure 3, in side section, cross section, modified, 15 partial cross section and modified cross section, respectively;

Figures 8a,b and c show side section through a diverter of Figure 1 (in fact Figure 1a) combined with the vortex valve of Figure 3 (a fountain element in 20 accordance with the present invention), in section in Figure 8a, in perspective view in Figure 8b and symbolically in Figure 8c;

Figures 9a to 9c show various ways of employing the arrangements of Figure 8, but as a control valve rather 25 than a direct fountain spray element;

Figures 9d to 9g show how various spray effects are achieved from arrangements of diverters and vortex valves;

Figure 10 is a section through a self oscillating 30 nozzle, useful in some embodiments of the present invention;

Figure 11 is a schematic illustration showing a wind detection and adjustment system, useful in a fountain system in accordance with the present invention;

Figure 12 is a schematic circuit diagram showing a manual control arrangement;

Figure 13 is plan view of a fountain system in accordance with the present invention employing some of 5 the arrangements illustrated in Figures 1 to 12;

Figure 14a to c show further circuit control elements useful in fountain systems according to the present invention;

Figure 15 is a plan view schematically illustrating 10 a fountain system in accordance with a further embodiment of the present invention;

Figure 16 is a detail of part of the system of Figure 15;

Figure 17 is a possible fluidic circuit arrangement 15 to give effect to the logic module shown in Figure 16;

Figure 18 is a diagram of a simpler logic circuit for a module receiving inputs from just two neighbours;

Figure 19 is a diagram of a circuit for a fountain in accordance with the present invention;

Figure 20 is a section through a swirl recovery 20 unit;

Figure 21 is a section through a swirl swamper;

Figure 22 is a diagram of a circuit modified from Figure 19 to provide manual control; and

Figure 23 shows a universal base.

Figure 1a shows an unvented bistable fluid amplifier (fluidic diverter 10), comprising a supply input 12, two control ports 14a,b, and two outputs 16a,b. The supply 30 flow is formed into a jet 17, which attaches to either the top or the bottom of a diverging section 18 of the diverter 10. Accordingly, the supply flow through the jet 17 will exit one or other of the outputs 16a,b. All

of the supply flow can be switched to either output (100% diversion) if brief control flows are imposed on the control ports 14a,b. If the outputs are unrestricted, flow can be entrained from the inactive output, so that 5 the outflow appears to be greater than the supply flow ("more than 100% flow diversion"). The control flow needed to switch the diverter 10 depends on the output restriction. Increasing restriction (thereby reducing the percentage flow diversion) reduces the flow needed to 10 switch the diverter (that is to say, the restriction increases the "gain", but reduces the "stability").

In Figure 1b, vents 20a,b are shown in modified diverter 10a. The vents 20a decouple the outputs 16a,b, from one another so that there is no flow entrainment. 15 Moreover, the amplifier 10a acts as a logic element (flip-flop or memory device). It can be connected easily to other similar elements to transmit signals, because the vents 20a,b isolate operation of each device in the overall circuit.

20 Figure 1c shows the symbol employed herein in circuit arrangements. The reference numerals are the same as those employed in Figures 1a. Indeed, the same reference numerals are applied throughout this specification to refer to essentially the same 25 components, sometimes modified with subscripts or superscripts to indicate modifications or different examples of the same unit.

Figure 1d shows a further diverter 10b, having a cusped splitter 22 between the two outputs 16a,b. The 30 twin cusps 22 promote a re-circulation zone and provide a highly stable flow field. This is because, even should the active outlet 16a or b be blocked, a re-circulating

flow can remain attached to the adjacent side wall of the diverging section 18. When the block is removed, flow continues down the same branch.

GB-A-1297154 and 1363762 both disclose the use of a fluidic diverter to provide oscillating flow. This is done by interconnecting the control ports of the diverter, as illustrated in Figure 1e, where the control ports 20a,b are interconnected by a hose 24. The diverter must be suitably designed (ie not a high stability type) and the outputs must be restricted, as shown at 16'a,b). Sufficient restriction should be made of the outputs 16'a,b to ensure 100% flow diversion. The frequency of oscillation is determined by the inertia of the flow through the control loop 24, and the pressure difference induced between the control ports by the main flow jet 17. Increasing flow increases the pressure differential and the result is that frequency is closely proportional to the flow. Importantly, the time constant can be set by inertia and resistance (without the need for compliance - ie elasticity). Consequently, an incompressible fluid, such as water, can fill the control loop 24 and produce a reliable dynamic response. In general, the longer the control loop 24 is, the lower the frequency of oscillation will be. On the other hand, the control loop 24 cannot be so long that its resistance prevents the necessary flow to build-up and switch the diverter 10c.

It is important to expel all air in the control loop 24, and one way of doing this is to provide a bleed tap (not shown) near the middle of the control loop 24. This works provided that the pressure in the control loop is greater than atmospheric. If the pressure is lower, then

a small water feed into the control loop to purge the loop of air may be required.

Figure 1f shows a diverter 10d in which restricted outputs 16'a,b are provided with branches 26a,b that are 5 fed back into the control ports 14a,b. The restrictions of the outputs ensure a strong feedback signal. These set the frequency by way of a predominantly inertial time constant (like the control loop 24 mentioned above). However, if compliance is introduced into the feedback 10 path, this influences the time constant. Indeed, increasing elasticity (or increasing inertance) decreases the frequency. If elasticity is minimized, the inertial time constant is dominant and, like the control loop oscillator 10c, the frequency is closely proportional to 15 the flow.

In Figure 2a, a two stage fluidic bistable amplifier 30 is shown. Here, a first diverter 10 corresponds with any of the diverters discussed above with reference to Figures 1a to f. However, its outputs 16a,b form the 20 control ports 14'a,b of a second diverter 10e. This is shown in symbol form in Figure 2b. Such an arrangement can provide both pressure and flow gain. Typically, diverter 10e is bigger than diverter 10, especially if the diverters are unvented devices.

25 Various logical functions can be produced by simple chains of bistable amplifiers. Four amplifiers can be used as two stages of a shift register. See, for example, Figure 2c. Here, two-stage amplifiers 30a,b are connected in series, each serving as memory elements 30 containing one bit of information each. Amplifiers 10<sub>1</sub> and 10<sub>3</sub> are memory elements containing one bit of information each, whereas amplifiers 10<sub>2</sub> and 10<sub>4</sub> act as

control gates. If the supply flow to the control gate is zero, there is no transmission of the state of amplifier 10<sub>1</sub> to amplifier 10<sub>3</sub>. However, when a "shift signal" is fed to gates 10<sub>2</sub> or 4 the state of flow through the 5 preceding amplifier 10<sub>1</sub> or 3 is transmitted to the next element in turn (ie diverter 10<sub>3</sub> or beyond diverter 10<sub>4</sub>).

Thus, if the supply flow to diverter 10<sub>1</sub> is presently directed to the upper output (ie in the direction of the arrow A) then, when a shift signal is sent to supply 12<sub>2</sub> 10 of diverter 10<sub>2</sub>, its output will be switched by the A output of diverter 10<sub>1</sub>. It will be switched into an output in the direction of the arrow B from diverter 10<sub>2</sub>. This will serve in turn to switch the supply entering 15 diverter 10<sub>3</sub> from its input 12<sub>3</sub> to the direction C, which it will then maintain even if the shift signal 12<sub>2</sub> into diverter 10<sub>2</sub> should subsequently cease. Likewise, the preceding state of diverter 10<sub>3</sub> would be passed on to subsequent elements of the logic circuit by the diverter 10<sub>4</sub>.

20 In a chain of more than two or three amplifiers, the flow gain may be substantial. In that event, some of the amplifiers would typically be vented devices.

Such chains of amplifiers can be controlled in various ways. For example, the gating signals to the 25 control amplifiers 10<sub>2</sub>, 10<sub>4</sub> can be activated in anti-phase (ie one on and the other off) thereby giving very tight control of the progress of signals through the chain. The same surety can also be achieved by restricting the signal strength transmitted from the memory amplifiers 30 10<sub>1</sub>, 10<sub>3</sub>. Signals can only transmit when the gate amplifiers accept the weak signal, and then boost it to control the next amplifier. This onward transmission

only occurs when the gate amplifiers have a high supply flow, but they are then immune from the weak signals coming from the preceding memory amplifiers. Hence a shift register can be made using two amplifiers per 5 stage.

Various sequences of signals can be generated by feeding back signals from the output to the input of a shift register. By feeding back simple logic functions (for example exclusive-or) so called maximum length 10 sequences can be generated (meaning the maximum possible length of bit sequence before repetition from the given number of memory elements in the shift register). Hence, complicated sequences of events can be controlled. Figure 2d shows a multi-stage fluidic shift register 30'.

15 Turning to Figures 3a to d, a vortex valve 40 is shown having a supply flow input 42 and a control flow input 43. The input 42 is received in a housing 44, it being sealed thereto by an end cap 46. Inside the housing 44, the supply input is perforated with regularly 20 spaced holes 48 (spaced both axially and circumferentially) so that the flow enters an annular duct 50 formed between the input pipe 42 and the housing 44. The input pipe 42 is sealed at its end by a centre body 52 that defines one side of a vortex chamber 54. 25 The other end of the vortex chamber is closed by a nozzle plate 56 having a central nozzle 58.

The control flow input pipe 43 is connected to the nozzle plate 56 and is terminated by a tangential port 60 that connects the pipe 43 with the vortex chamber 54.

30 In the absence flow in the control pipe 43, flow in the pipe 42 exits through the holes 48 and flows along the annular duct 50 and enters the vortex chamber 52 in a

radial direction from around the entire circumference of the centre body 52. Accordingly, there is no circumferential component of the flow. It is entirely radial, as shown by the arrows in Figures 3a and c. 5 Accordingly, the output from nozzle 58 may be a coherent, non-swirling jet that will exit the nozzle 58 as a clean column of liquid, with no spray or break-up.

However, if there is no supply flow 42, but only flow in the control pipe 43, then the vortex chamber 54 10 is filled by supply through the tangential port 60. So that there is a swirling flow in the vortex chamber 54 as shown by the arrows in Figure 3b. In this event, the flow out of the nozzle 58 has substantial swirl and exits nozzle 58 as a coned spray. The cone angle is dependent 15 on the geometry of the nozzle and the degree of swirl in the vortex chamber 54.

Accordingly, depending on whether flow to the vortex valve 40 is through the supply input 42 or the control input 43, the exit from the nozzle 58 is either as a 20 coherent jet or as a fine coned spray.

Referring to Figures 8a to c, the vortex valve 40 is shown there used in conjunction with a diverter 10 to form a basic fountain 50 in accordance with the present invention. In its simplest form, the fountain 50 25 comprises a diverter 10 as described above with reference to Figure 1e. That is to say, one in which the control inputs 20a,b are interconnected by a control loop (not shown in Figure 8a). In this event, the flows to the respective outputs 16'a,b simply oscillate, so that flows 30 to the inputs 42,43 of the vortex valve 40 alternate with respect to one another. Thus, the output from the outlet

nozzle 58 oscillates between a straight jet and a coned spray.

In Figure 8b, it can be seen that diverter 10 has a rectilinear cross-section. This favours effective switching between the respective outputs, both by virtue of the control inputs 20 being across the entire section of the supply 12, as well as the jet flow having greater surface of the diverging walls 18 over which to attach thereto. However, in a practical embodiment, there is likely to be a smooth transition between the round supply, control and delivery tubes connected to the diverter 10, and the rectilinear sections of the diverter itself. The symbol for the switched vortex valve 50 is shown in Figure 8c.

Returning to Figures 4a to c, a nozzle plate 56a is shown in Figure 4a. A nozzle body 57 can be screwed into a threaded aperture 55 of the nozzle plate 56a. The nozzle body 47 has the nozzle aperture 58 and this can be shaped to provide the desired jet. Where the two forms of jet are a swirling conical flow sheet, or a coherent jet, these are most readily accommodated by a smoothly chamfered inlet 59 of the nozzle 58 and a sharp exit 61. In Figure 4b and c, a nozzle body 57' is here held in place by a threaded retaining ring 63 screwed onto a modified nozzle plate 56b, which is provided with an O ring seal 67.

Turning to Figure 5a, one embodiment of retaining ring 63' is shown having a pin 69 projecting therefrom and to which a swirl deflector disc 71 is connectible. Disc 71 is provided with a central aperture 73 through which jet flow from nozzle 58 can pass unimpeded. However, when a diverging coned sheet flow (suggested by

arrow 75 in the drawings) emanates from the nozzle 58, it is deflected by the disc 71 and evolves more as a horizontal spray, even more distinct from the jet than the coned spray. Alternatively, an entirely spray 5 destructive shroud 71' can be connected to the pin 69. The shroud 71 entirely contains and destroys the conical spray 75 so that the output from the nozzle 58 appears only to comprise a pulsating jet. If that is very coherent, its appearance is very appealing, emphasizing 10 the motion of the water in an arcing flow.

Figure 5c shows how the disc catcher 71 may be implemented with a screw in nozzle 57'. Here, a disc 72 is formed integrally with the nozzle body 57' and to which the pin 69 is connected. To the pin 69, deflector 15 disc 71 or shroud 71' can be connected as desired.

Referring to Figure 6, various forms of nozzle plates 57' are shown.

Figure 6a shows a basic nozzle 58 that gives a conical spray and a good coherent jet. In Figure 6b, 20 nozzle 58b has a chamfered exit so that a flat or very wide spray is delivered. However, it is more difficult for the jet to remain coherent, so that any swirl is more likely with this arrangement to lead to break-up of the jet. In Figure 6c, the nozzle 58c is in the form of a 25 flat slit across the face of the nozzle plate 57'. This results in a flat, triangular sheet-jet. In Figure 6d, a stepped bore nozzle 58d provides a very tight spray and a good jet. Figure 6e shows a multi-jet nozzle 58e. Figures 6f and g show a modified nozzle plate 57" that is 30 provided with a threaded bore 55' to receive screw-in nozzle bodies 58 similar to those described above with reference to Figure 4a.

Turning to Figure 7a to d, a modified vortex valve 40' is shown in which the control pipe 43' now surrounds the housing 44 and has a number of tangential control ports 60'. However, to direct the flow tangentially, the 5 wall of the housing 44 has to have a substantial thickness, so that a tangential flow direction can be provided by the ports 60'. Alternatively, vanes 75 may be disposed across the wall 44, so that flow from the annular control duct 43' into the vortex chamber 54 is 10 caused to swirl by those vanes 75 on passing through the openings 60'. Also, as shown in Figure 7c, straightening vanes 77 can be provided on the centre body 52 so that flow through the supply pipe 42 can be maintained absolutely axial.

15 Referring to Figures 9a to g, various combinations of the foregoing components are illustrated. In Figure 9a, the switched vortex valve 50' is shown delivering an output outflow on line 76 that is led to another device or system. The effect of the diverter 10/vortex valve 20 40' combination is that the supply flow 12 is modulated at the output 76 by the control flows 20. When the vortex valve 40' is supplied by output 16b of the diverter 10, then no vortex swirl is produced in the vortex chamber 54 of the vortex valve 40'. Therefore, a 25 high flow rate is seen at the output 76. On the other hand, if the output of the diverter 10 is through line 16a, then this enters the vortex valve 40' tangentially. This causes a vortex in the chamber 54 and so increases the resistance of the valve to flow. A relatively small 30 output flow is then seen at the outlet 76.

In Figure 9b, a diverter 10 is shown with its outputs 16a,b connected to two vortex valves 40a,b. Each vortex valve has its own radial supply 42a,b so that,

depending on the switched state of diverter 10, vortex valves 40a,b will alternate between respective jet flow and spray flow. In Figure 9c, the arrangement is as in Figure 9b except that the vortex valve 40'a,b are as shown in Figure 9a, and are used to provide flow for another device or system from their outputs 76a,b.

In Figure 9d, two diverters 10a,b are used to control a single vortex valve 40" having opposed control flow inputs 43a,b. This provides for potential modes of operation depending on the four possible combinations of the outputs from diverters 10a,b. Indeed, the four output states of the flow from nozzle 58 are described in the Table I above for amplifier B.

In Figure 9e, a variation is shown in which the control nozzles 43a, 43'b of vortex valve 40" are in the same direction. Table I above describes the outflow through the nozzle 58 of the vortex valve 40" (amplifier A), depending on the states of outputs of the diverters 10a,b.

Figure 9f shows the symbolic representation of the arrangement described with reference to Figure 1e above in which a control loop 24 is employed to provide oscillatory flow at the control inputs 20a,b of diverter 10. Indeed, the arrangement shown in Figure 9g is perhaps the simplest embodiment of fountain in accordance with the present invention, in which the input supply 12 is connected to a source of water under pressure (eg mains supply) and the output from the nozzle 58 is either a spray or a single jet. Such an arrangement is simple and inexpensive to manufacture and yet provides an alternating display not presently available so simply.

Figure 9g shows an arrangement as described above with reference to Figure 9e, but where control loops 24a,b for the two diverters 10a,b are provided, each of different length. Each diverter switches with a 5 different frequency, therefore, and this results in a somewhat random, or cyclic, appearance to the four output states from the nozzle 58 of the vortex valve 40".

Figure 10 illustrates a self-oscillating vortex nozzle 80 comprising flat top and bottom walls 82, a 10 circular vortex chamber 84 and an input chamber 86. The input chamber 86 has a supply port 88 in the wall 82 and the vortex chamber 84 has a central outlet nozzle 90 disposed in the wall 82 that is opposite the wall containing supply port 88. A waist 92 defines the 15 interface between the inlet chamber 86 and the vortex chamber 82. It is found that, in operation, flow into the inlet chamber 86 transitions into the vortex chamber 84 and oscillates between direct flow (that issues from the nozzle 90 as a jet), and swirling flow (resulting in 20 a spray issuing from the nozzle 90). The swirling flow is first clockwise, then anti-clock wise and switches back and forth.

Referring now to Figure 11, a wind detection system 100 comprises a vertical nozzle and water jet 102 and a 25 surrounding catcher basin 104. The diameter of the basin 104 is designed to be so small that only wind of less velocity than a certain, predetermined velocity will permit the water issuing from the nozzle 102 to be caught by the basin. Wind of any greater velocity will deflect 30 the jet so that it falls beyond the edge of the basin 104. The catcher 104 feeds a vertical columnar collector 106. The wind state is detected by a fluid amplifier 101 having a small supply flow 121. Control input 20a of the

amplifier 10<sub>1</sub> is provided by the collector 106. At low wind speed, the control signal here is strong, and the amplifier is switched to output 16b. Control input 20b is supplied by a feedback bias from output 16b, but the 5 feedback flow is insufficient to overcome the control flow from the wind detector during low wind conditions. However, should a high wind develop so that the catcher 104 empties and no flow comes from the collector 106, the feedback bias from output 16b is sufficient to switch 10 diverter 10<sub>1</sub>. Its output then appears on output 16a. The outputs from diverter 10<sub>1</sub> are further amplified by a second bistable amplifier 10<sub>2</sub>. More stages could be added to provide control signals to the water supply system, for example, to the fountain system.

15 With reference to Figure 12, a manual control system is provided by a diverter amplifier 10 provided with a supply 12 that has two branches 13a,b that supply control inputs 20a,b of the diverter 10. Both branches 13a,b are controlled by restrictors R<sub>1</sub>, R<sub>2</sub>. However branch 13a is 20 provided with a further restrictor R<sub>3</sub>, and, between restrictors R<sub>1</sub> and R<sub>3</sub>, a selectively blockable vent V is provided. Under normal, unblocked conditions, restrictor R<sub>3</sub> and vent V conspire to ensure that substantially no flow is provided at control 20a. In that event, diverter 25 10 is switched by the flow through restrictor R<sub>2</sub> and control port 20b so that its supply 12 exits on output 16a. However, restrictors R<sub>1</sub> to R<sub>3</sub> are arranged so that, should vent V be selectively blocked, a more powerful 30 flow is provided by control port 20a, so that diverter 10 is switched to output 16b. Indeed, in this respect, branch 13b provides a reset signal in the absence of activation of branch 13a by blocking vent V. However, an alternative arrangement would be to duplicate branch 13a

in branch 13b, whereupon a bistable arrangement would be provided capable of being switched by blocking either of the vents.

Figure 13 discloses a fountain system 110 embodying 5 the present invention and employing some of the components described above. Here, a main pump 112 supplies water under high pressure. The output 114 immediately branches into a high pressure branch 116 and a branch leading to a jet pump 118 that entrains flow 10 from a source 120 to provide a high flow branch 122. The high flow branch supplies two vortex valves 40a,b in an arrangement as described above with reference to Figure 15 9b. The vortex valves are controlled by a diverter 10 which is operated in a mono-stable mode under the control of a wind detector 100, and substantially as described above with reference to Figure 11. The only modification is that the bias is provided by a branch of the high pressure supply 116. A signal amplifier 124 outputs the signal from the wind detector 100 to the diverter 10.

20 The arrangement is such that, in low wind conditions, vortex valve 40b is set to high resistance so that the high flow supply in line 122 is impeded and results in a low flow supply in output 126. However, 25 radial flow is permitted through vortex amplifier 40a, so its output 128 is in high flow during low wind conditions.

Output 126 supplies a ring 125 of three fountain devices 50a,b,c and a central fountain 50d, all of which are substantially as described above with reference to 30 Figure 8. Whereas fountain 50d may be under automatic control by a closed loop, for example (as described above with reference to Figure 9f) high pressure line 116 may

also supply a manual control device 130 (operating substantially as described above with reference to Figure 12). This is arranged to control the ring of fountains 50a,b,c.

5 On the other hand, output 128 from the vortex valve 40a supplies two outer rings 127 of devices, an inner ring 129 of oscillating valves 80 (substantially as described above with reference to Figure 10) and an outer ring 131 of diverter fountains 10'. Here, the diverter  
10 outputs 10' are themselves provided with nozzles to deliver alternating jets of water. Again, the high pressure supply 116 is fed to a signal generator 30'', which controls the sequencing of the diverter jets 10'. The signal generator 30'' may be a sequence generator  
15 controlling all the diverters 10' so that they switch in sequence to produce a "Mexican wave". Alternatively they may be switched in phase.

Turning to Figure 14, the diverters 10' of the ring 131 in the fountain system 110 of Figure 13, may include  
20 an integrated, small pilot amplifier 10''. This would enable small signal flows sent from the central control unit 30'' to switch the diverters 10'.

Using the concept of piloted fluidic display devices, the control sequences could conceivably be  
25 implemented by the display devices themselves, if suitable interconnections were made. For example, with an array of N diverters and switched vortex valves, correct interconnection feedback would enable the array to go through a sequence of  $2^N$  different combinations of  
30 right/left events (diverter fountains 10'), or spray/jet events (diverter vortex amplifier combinations 50) before repetition. In effect, the individual display devices

(albeit supported by their pilot stage) would constitute elements of the shift register sequence such as described above with reference to Figures 2c and 2d.

A further advance is shown in Figure 14b and c,  
5 which would be to attach a logic module 132 to a diverter 10. In Figure 14b, the diverter 10 comprises the fountain element itself. On the other hand, in Figure 14c, the diverter is part of a switched vortex valve 50. In either event, the logic module has its own supply 134  
10 that appears at one of its outputs 136 forming the control inputs of the diverter 10. Multiple inputs from other sources can be integrated to provide an output on either line 136 depending on which inputs are active.

With an arrangement such as this, an array 150 of  
15 fountain devices can be internally controlled. In Figure 15, a central array of switched vortex valves 50 are shown with a surrounding array of diverters 10. Each device is connected by input and output signals to the surrounding eight devices. At the edges of the display  
20 150, signals from one side are transmitted to the opposite edge, so that a topological sphere is provided.

Turning to Figure 16, a single fountain element 10/50 is illustrated having eight surrounding elements 1 to 8. Each of the surrounding elements has a diverter  
25 output A or B. The A branches of surrounding fountain elements 1, 6, 7 and 8 are connected to inputs 1, 6, 7 and 8 respectively of logic controller 132 of the device 10/50. The remaining surrounding devices 2, 3, 4 and 5 have their B outputs connected to inputs 2 to 5 of logic  
30 controller 132. How logic controller 132 is configured is a matter for discretion and design choice, but one

possible switching regime is illustrated in Table II below.

Number of Active Inputs	Current State	Consequent Output State	Next
1,2,4,5,6,7 or 8	Left	Stay Left	
1,4,5,6,7 or 8	Right	Switched Left	
3	Left	Switched Right	
2 or 3	Right	Stay Right	

Table II

In any event, depending on the logic mode chosen,  
5 the output of device 10/50 is to one of its two outputs 136, that is to say, A or B. It is to be noted that the outputs A,B of the device 10/50 each have four branches leading to one each of four of the eight surrounding devices 1 to 8, providing inputs to their logic modules  
10 132<sub>1</sub> to 132<sub>8</sub>.

When connected in this way, the array emulates a classic cellular automaton ("Life", created by John Horton Conway). As a result, the fountain display 150 could replay any of the well established complex (and 15 sometimes perpetual) sequences. Further possibilities in cellular automata are provided by Stephen Wolfram ("A New Kind of Science" ISBN 1-57955-008-8, Wolfram Media Inc, 2002) who has recently explored and completely characterised many hundreds of millions of binary 20 algorithms. In principle these could be implemented by advanced fluid fountains.

Conceivably, very large arrays of devices could be assembled which would undergo the highly complex "Life" and "Death" phases of cellular automata. The onlooker 25 would see waves, whirls, spasms and inactivities, typical

of systems which currently only exist on computer driven video display units.

Figure 17 shows schematically a possible arrangement of a logic control module 170 of the type schematically illustrated as module 10/50 in Figure 16. This arrangement reproduces the "Life" automaton referred to above. It has eight control inputs  $C_1 - C_8$ , each supplied by a neighbour's active output. The inputs are combined in a network of Y-joints 172, which produces a summation of the signals. This summed signal is applied to three monostable threshold gates, TGa, TGb and TGc, through weighting restrictors  $R_1$  which set the signal strength that causes each gate to switch. Gate TGa is caused to switch inactive if 2 or more inputs  $C_{1-8}$  are active, gate TGb is switched inactive if 3 or more inputs are active, and gate TGc is switched by 4 or more of inputs  $C_{1-8}$  being active. Logical processing of the resulting logical functions is then done by fluidic logic devices: two NOR-gates B and S, and two bistable (memory) devices C and N. Bistable N has two control inputs on one side equivalent to an OR function of those inputs. Bistable C holds the current state *Alive* or *Dead* of the "cell" represented by the whole circuit. Signals from bistable C are combined with the logical functions from the threshold gates in the NOR gates B & S. NOR gate B generates a signal implying "birth" of a cell from an originally dead state. NOR gate S generates a "sustain" signal which maintains the existing live state of a cell. These signals, which both generate a live state for the next time phase of the automaton, are fed to the next-state bistable N. Bistable N holds the logical state ready for transfer to the "current-state" bistable C via feedback lines F connecting to the input control ports of bistable C.

"Death" is produced by a bias signal BS fed from the common fluid power supply S via a restrictor  $R_2$ ; this resets bistable N to the "die" command, unless countermanded by the control inputs from NOR gates B or 5 S.

The cell and the overall cellular automaton exists in a sequence of discrete states controlled by a centrally generated clock signal TS. At regular intervals this activates bistable N and sends strong 10 signals to change the state of bistable C. By attenuating the signals from N by restrictors (not shown) in the feedback lines, only a very large transfer signal is able to effect the signal transmission. At this high supply power the bistable N is immune from the relatively 15 weak logic signal S from the NOR gates. Hence race hazards are avoided (signals racing round the signal feedback loop out of synchronism with the clock signal).

The fountain display element is bistable C or some other device controlled by it. The cell communicates to 20 others in the array by *LIVE* (active) signals sent from the appropriate output of bistable C.

Figure 18 shows schematically a possible arrangement of a fluidic logic control module 180. This represents one "cell" of a different cellular automaton to that 25 described above. Here, the logical algorithm and the corresponding circuit implement the "rule 30" automaton discovered and described by Stephen Wolfram, (reference above). The cell exists in a sequence of discrete states, each determined by the state of the cell and its 30 two neighbours. The current state of the cell, *ALIVE* or *DEAD* is held in bistable memory element CC. A signal from this, and input signals L and R from left and right

neighbouring cells, are processed by a logic circuit consisting of an active OR-gate AO and an exclusive OR-gate EO. The active OR-gate AO is a fluidic monostable switching device and therefore does not attenuate the signal. The exclusive OR-gate EO is not active and therefore also does attenuate the signals.

The output of the exclusive-OR gate EO is the signal fed to bistable memory element NN holding the next state for the cell. The signal from the exclusive OR-gate signifies "ALIVE" for the next state. A bias signal returns the bistable NN to its "DEAD" state in the absence of an output from the exclusive-OR gate. The time-sequence of states for the cell, and the whole automaton, is controlled by a centrally generated clock signal TS. At regular intervals, this activates bistable NN and sends strong signals to change the state of bistable CC. By attenuating the signals from NN by restrictors (not shown) in the feedback lines FF, only a high pressure transfer signal is able to effect the signal transmission. At this high supply power, the bistable NN is immune from the relatively weak logic signals from the exclusive-OR gate and the bias signal. Only when TS is very low or near zero can its state be controlled by the bias or exclusive OR-gate. However at this low supply pressure bistable NN cannot affect bistable CC. This ensures that the "current" and "next" states are separated by finite time periods and that signals do not race around the system out of synchronism with the transfer signals.

Signals to the cell's neighbours are provided by bistable CC. As part of a fountain, bistable C might be a jet diverter, so acting as a display element itself, or it might control other diverters and/or vortex valves.

Wolfram's "rule 30" automaton is defined in terms of a one-dimensional (a line) array and the foregoing description conforms to that definition. Wrapping up linearly connected cells to form a square or other two-dimensional figure can produce two-dimensional arrays. Other two-dimensional arrays can be produced by slight modifications to the interconnections within and between cells. As an example, the next-state bistables could feed signals to cells in a neighbouring row, rather than the internal feedback to bistable CC just described.

The logical function generated by the circuit is

$$\text{Next-State} = L \underline{\vee} (R \vee \text{Current-State})$$

where  $\vee$  signifies the OR-function and  $\underline{\vee}$  signifies exclusive-OR

The resulting function is shown in Table III below in which 1 signifies "alive" and 0 "dead."

<b>L</b>	<b>Current State</b>	<b>R</b>	<b>Next State</b>
0	0	0	0
0	0	1	1
0	1	0	1
0	1	1	1
1	0	0	1
1	0	1	0
1	1	0	0
1	1	1	0

Table III

Turning to Figure 19, a diverter 10f is shown in a circuit 30f in accordance with an embodiment of the present invention. Here, a diverter with fixed construction, particularly a diverter with a fixed length and diameter of control loop 24f, the frequency of

oscillation is a function mainly of supply flow 12f. Apart from changing the supply flow, the frequency is difficult to adjust. However, if a small amount of flow is added to or extracted from the control loop, the frequency can be altered. A reason for doing this is to optimise the visual effect of the display. Flow can be added by tapping-off some of the supply flow, which is always at a higher pressure than in the control pipe via valve 1. Flow can be passively bled to atmosphere or 10 pond through valve 2 if the control loop pressure is above that of the atmosphere or the pond.

Adding flow decreases the frequency, and extracting flow increases the frequency. It is not always possible to simply bleed flow from the control loop, however, 15 because for a simple diverter not connected to a vortex valve, the control loop pressure is often too low or may even be sub-atmospheric. A passive bleed valve 2 would then merely admit air, which would be detrimental.

When the diverter is connected to a vortex valve, 20 the control loop pressure is usually higher than atmospheric, so bleeding flow is practical. For the cases where the control loop is at low pressure, a water driven jet pump or ejector (not shown) could be used to suck flow from the control loop 24f (via valve 2).

25 The ability to inject or extract control loop flow has the added benefit that it can assist in purging the control loop 24f of air when initially switched on. Also it serves to wash debris from the control loop.

In order for the control loop oscillator to 30 oscillate regularly, the output resistance on the diverter (ie on both outlets 16a,b equally in a symmetrical diverter) must be correctly adjusted. If the

resistance is too small (i.e no blockage, or a virtually free exit path), the diverter may cease to oscillate because sensitivity or "gain" of the fluidic amplifier (fluidic diverter) drops at high outflows. As the outlet 5 resistance is increased, gain increases and oscillation is easier to ensure. However, if the outlet resistance is too high, the flow cannot be diverted (in the limit at very high resistance, it splits equally between the two outlets 16a,b), so a compromise must be found.

For the diverter 10f acting as a fountain, the two outlets are, in fact, the fountain jets. They are easily accessible and can be adjusted or exchanged to obtain the best effect. For the diverter-switched vortex valve, the outlet resistance is built-in to the overall system. The 10 tangential nozzle (60, Figure 3a, for example) in the vortex valve 40 forms one diverter outlet resistance (which can be well defined at the design stage), but the other outlet 50 is simply the non-swirling supply duct, typically along the axis of the vortex valve. If this 15 resistance is too small, poor oscillation may occur. Hence it is important to ensure that, if no adjustment can be made, adequate restriction is built in. Alternatively, "fine tuning" may be provided during final 20 commissioning of a device. Such tuning could be made by 25 various known arrangements such as needle-, gate-, butterfly- or ball- type valves.

Two additional methods of modifying the outflow apply to the switched vortex device, as shown in Figures 20 and 21. In the first method, the swirling flow (in 25 the vortex mode of operation) is captured in an annular plenum 175 of vortex valve 56f. An annular diffuser 177 leads from the exit nozzle 58f, which is either flat or 30 conical, as shown. Dynamic pressure in the swirl flow is

converted to static pressure in the plenum 175. Nozzle(s) 179 fed from the plenum produce a jet or jets during the vortex phase of operation. The jets 179 can be arranged around the central axis of the vortex valve pointing 5 upwards and outwards to give an intermittent "crown-like" or "flower-like" spray of water on every switching cycle of the device. Alternatively a pressurised water signal can be drawn from the plenum via a pipe to act as a switching signal for other devices. To recover pressure 10 successfully, the annulus 177 must be narrow and its entry point close the vortex nozzle exit 58f, as shown.

The second method involves surrounding the exit nozzle 58g (see Figure 21) from the vortex valve with a cup-like container 181. Water can be made to submerge 15 the nozzle, thereby modifying the appearance of the outflow. A deeply submerged nozzle produces an attenuated outflow, particularly in the vortex state. The spray can be completely suppressed if desired.

If the cup has a small volume, the contents can 20 quickly get swept away by the outflow, so unless the water is replenished, the effect is transient. If the cup has a large area and volume, the water may be self-replenishing and the effect permanent. If water flow to and/or from the cup is controlled by some independent 25 means then this enables the appearance of the fountain to be controlled, perhaps by onlookers or by automatic, even fluidic, methods. For example the cup 181 may be provided with an overflow 183, whose exit may be controlled. When full, the cup may only permit the 30 central jet to exit, but when allowed to empty, both the central jet and vortex, modified as the cup fills, may be seen.

A fluidic diverter tends to suck flow into its control ports, even when the outputs are loaded by significant restrictions. It is easy therefore, in principle, to switch manually a diverter (ie one without a closed control loop) simply by blocking one of the control ports. This method has disadvantages however. In a water flow system, the inflow to the control should be water, so the control port to be blocked should be submerged. If air enters, operation is very erratic. Submergence might be inconvenient for many applications. Furthermore, even if submerged, the sucked-in control flow might be a source of contamination by unfiltered pond water, for example.

A better method of manual control is shown in Figure 22. This uses a system of restricted feeds and bleeds to enable the blockage of a sensing port to switch the diverter.

In the absence of manual input, small flows feed from tappings 185 of the supply 12g via restrictors 1a and 1b to the control ports 14a,b. Flow is restricted by restrictors 2a and 2b, a slight excess being bled through restrictors 3a and 3b to atmosphere along lines 187a,b. These bleed flows ensure that air, or external pond water, does not enter the system. The restrictors are set to enable the diverter to be stable when there is no manual input.

Blocking one of the bleeds 187a,b manually causes all the flow from the associated flow feed to enter the control port and when properly adjusted, to switch the diverter. The output of such a manually controlled diverter can, in principle, be communicated to any other fluidic device in an array. Indeed, the arrangement could

be arranged to be monostable, with only one bleed (eg 187a) being manually operated, the other being permanently sufficient to maintain the flow to output 16a while bleed 187a is unblocked.

5 A "universal base" system is shown in Figure 23. Here, a diverter is embedded in a rather sturdy, and perhaps massive, base block 190 of cement or similar rigid material. Both upward 192, and horizontal 194, outlets are incorporated. Normally, unused outlets would 10 be blocked by a stopper (not shown). The upward outlets 192 can have pipe-mounted nozzles 196 attached, or can feed a vortex valve 198 to produce the alternating spray-jet display. In both cases, the base is sufficient support. Outlying nozzle(s) 200 can be supplied for 15 connection to the horizontal outlets 194.

A purge valve 202 is fed from close to the supply inlet. A tee (not shown) in the control loop can be embedded in the base block. Thus the whole system constitutes a kit of parts which enables several display 20 options to be chosen.